# SEISMIC INSTRUMENTATION TECHNOLOGY SYMPOSIUM Palm Springs, CA • November 10-11, 2009

# Specifications For Building Instrumentation







Derek A. Skolnik Robert L. Nigbor and John W. Wallace

#### DAS SPECIFICATIONS

#### **SMIP Specifications**

- Recommended specifications for civil structures (buildings)
- Based on qualitative assessment and experience

Recommended Specification	ANSS (USGS 2005)	<b>CSMIP</b> (CGS 2007)	
Sensor Range ADC Resolution	±4g 16bits	± 4g 18bits	R (bits/g)
Sample Rate	200sps	200sps	S (sps)
Sample Sync	1% ∆t	0.2ms	T <sub>se</sub> (ms)
Reference Time	1.0ms	0.5ms	se (IIIS)
Clock Stability	0.1ppm	1min/month	

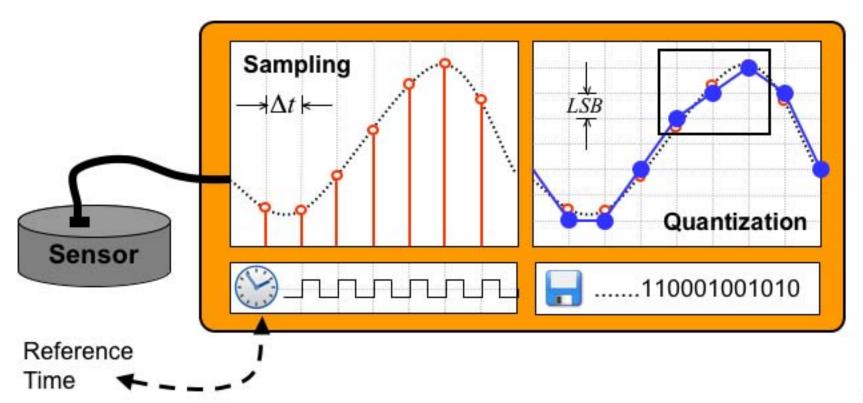
Guideline for ANSS Seismic Monitoring of Engineered Civil Systems, USGS Report 2005-1039
Integrated Tri-Axial Accelerograph, CGS/DGS SYSREQ 2007-TR

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# DAS SPECIFICATIONS

# Data Acquisition Systems (DAS)

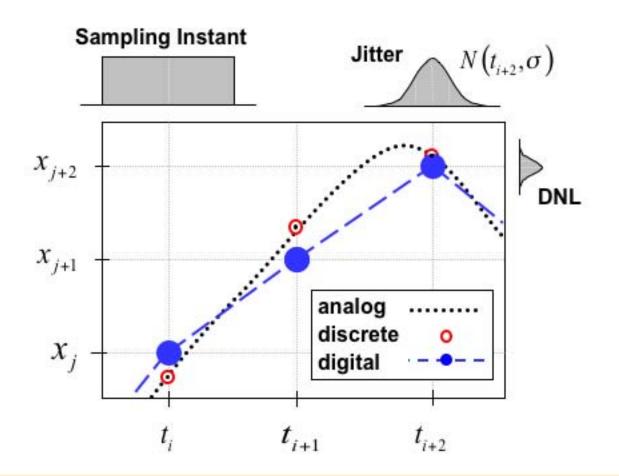
- Sampling sample rate  $(sps = 1 / \Delta t)$
- Quantization resolution (LSB = Range / 2 Bits)
- Time stamp for synchronization of multiple channels



# DAS SPECIFICATIONS

#### **Data Acquisition Errors**

- Sampling initial sampling instant and clock jitter
- Quantization Differential Non-Linearity (DNL)

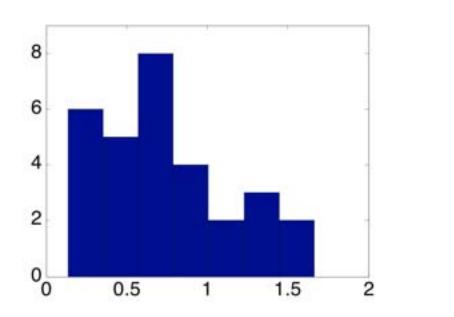


# OUTLINE

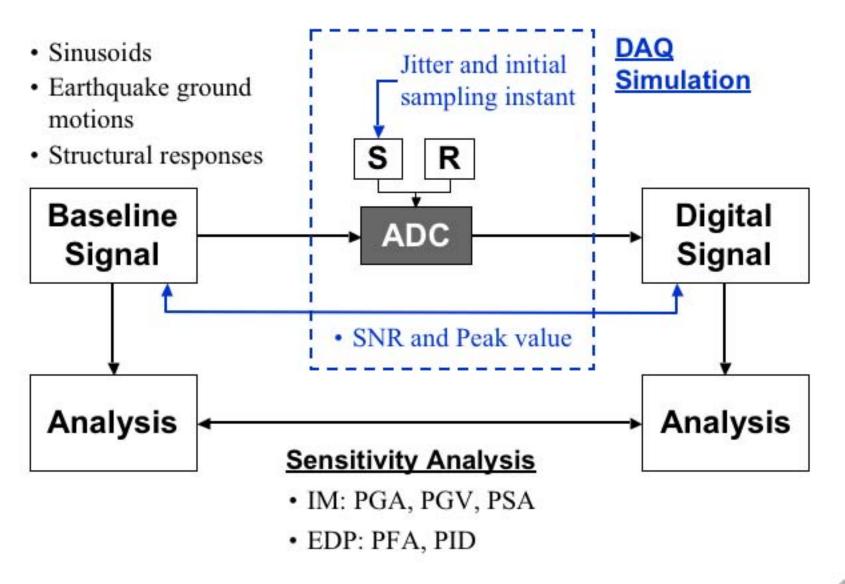
- Introduction
- DAS Specifications
- DAQ Simulation
- Sensitivity Studies
- Conclusions

#### **Baseline Earthquake Record Set**

- 30 EQ records downloaded from PEER, NCESMD, K-Net, KiK-Net, COSMOS
- Selected to capture broad nature of earthquakes
- Digitally enhanced to increase resolution: resample to 2kHz, zero-pads for filtering, band-pass filter 0.1-50Hz







#### **Clock Jitter**

- Independent of sample rate
- Can be neglected

Sinusoidal Signal

$$X(t) = A\sin[2\pi f t]$$

100sps

0.742

501/2

Sampled Signal

$$x_i = A \sin \left[ 2\pi f t_i \right]$$
$$t_i = i \Delta t$$

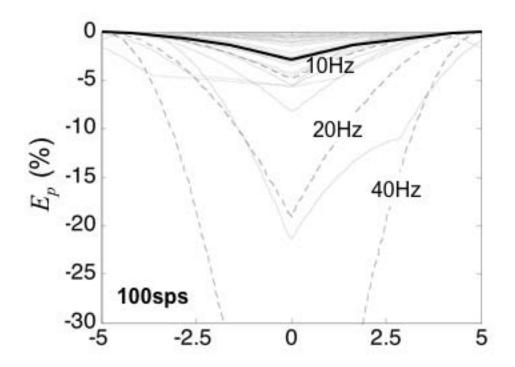
Jittery Sampled Signal

$$\overline{x}_i = A \sin \left[ 2\pi f \tau_i \right]$$

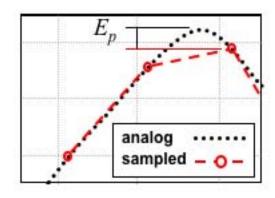
$$\tau_i \sim N(t_i, \sigma)$$

# Initial Sampling Instant

- Depends on sample rate
- Biased error always negative



Error in peak value  $(E_p)$ 



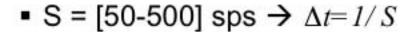
#### X = EQ record

1. 
$$t_0 \sim U(0, \Delta t)$$

2. 
$$t_i = t_0 + i \cdot \Delta t$$

3. 
$$x_i = interp(X @ t_i)$$

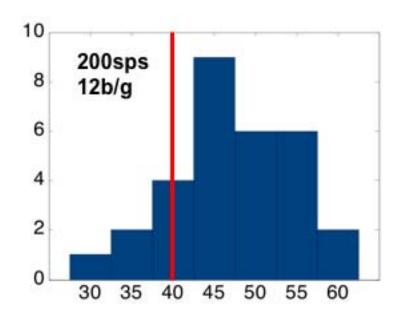
4. 
$$x_i = round(x_i / res) \cdot res$$



■ R = [6-24] bits/g 
$$\rightarrow res = g/2^R$$



30 40dB 50dB



# OUTLINE

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#### **OBJECTIVE**

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Determine minimum requirements for specifications of sample rate, resolution, and time synchronization

#### STRATEGY

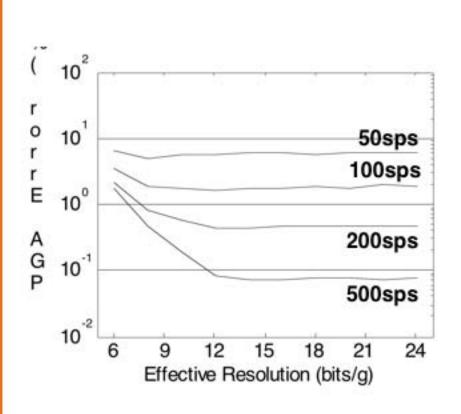
Quantify the sensitivities of ground motion intensity measures and engineering response quantities to DAQ

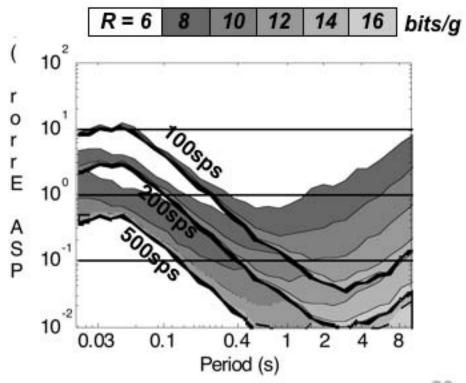
#### **APPROACH**

- 1. Understand how engineers use strong-motion data
- 2. Simulate the noisy DAQ process
- 3. Perform sensitivity analyses

# **Intensity Measures**

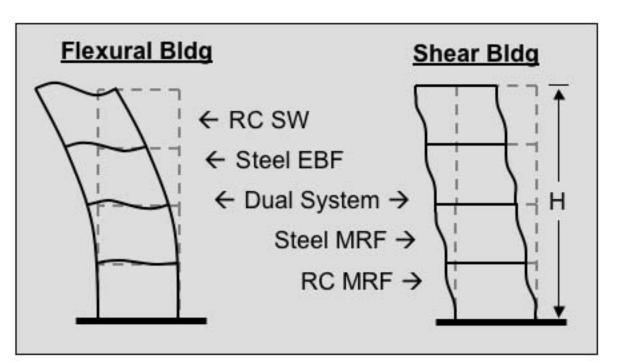
- PGA 100sps, 6bits/g for error less than 5%
- PGV 50sps, 8bits/g for error less than 5%
- PSA 200sps, 8bits/g for error less than 5%





# **Baseline Building Response Set**

- Simulate responses to baseline EQ record set by superimposed first few modal responses
- Assumptions: bounded by flexural & shear idealizations, uniform mass and stiffness,  $\zeta_n = 5\%$



$$\phi_n(x) = \sin\left[\frac{2n-2}{2}\frac{\pi x}{H}\right]$$

$$T_n = \beta_n T_1$$

$$\Gamma_n = \frac{\int_0^H m\phi_n(x)dx}{\int_0^H m\left(\phi_n(x)\right)^2 dx}$$

$$a_i = a_g + \sum_{i=1}^N \Gamma_n \phi_{ni} a_n$$

#### **Fundamental Period**

- Depends on building structure and height... sort of
- Based on real data from instrumented buildings
- Empirical conventions in code (ASCE 7) are lower bounds





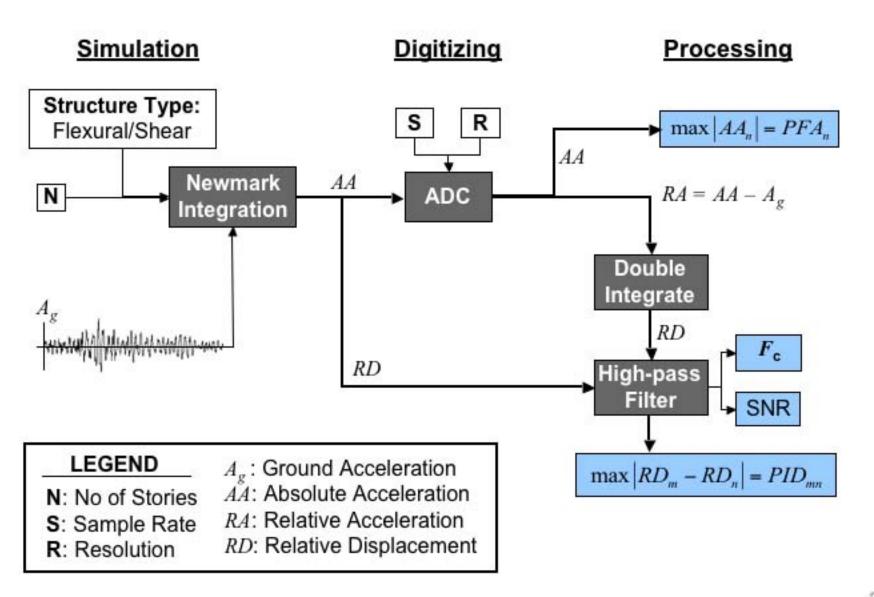
Steel MRF

$$T_s = 0.68 + 0.11N$$

$$T_f = 0.46 + 0.03N$$

ASCE 7-05 S12.8.2.1

$$T_a = C_t h_n^x$$



# Displacement (in)

# SENSITIVITY ANALYSIS



No correction SNR = -31dB

Detrend SNR = -16.3dB

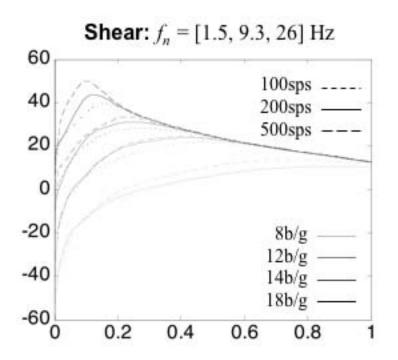
 $F_c = 0.01Hz$ SNR = -8.9dB

 $F_c = 0.1Hz$ SNR = 20.5dB

 $F_c = 1.0Hz$ SNR = 1.25dB

# **Optimizing Frequency Cutoff**

- High-pass 4<sup>th</sup> order acausal digital Butterworth filter
- A single floor of a 10-story bldg to one earthquake
- Resolution is important which corroborates Boore's (2003) findings of ADC quantization being a source of numerical drifts



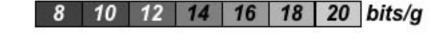
**Flexural:**  $f_n = [0.4, 1.2, 1.9] \text{ Hz}$ 

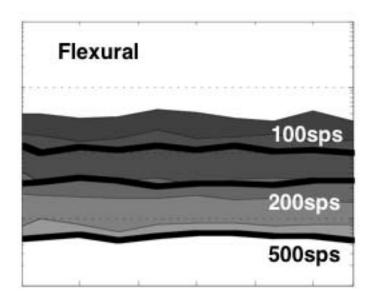
100sps ----200sps ----500sps ----

> 8b/g —— 12b/g —— 14b/g —— 18b/g ——

#### **Engineering Demand Parameters**

- PFA 100sps, 8b/g for error less than 5%
- PID 100sps, 14b/g for error less than 5%

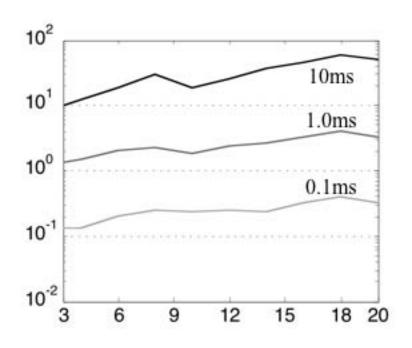




Shear

# **Time Synchronization Error**

- Sync errors are additional to digitizing error
- PID 200sps, 16b/g and sync to 1.0ms for total error < 5%</p>



10ms

1.0ms

0.1 ms

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#### CONCLUSIONS

Specification	ANSS (USGS 2005)	<b>CSMIP</b> (CGS 2007)	Recommend (Skolnik 2009)
Range	±4g	±4g	±4g
ADC Resolution	16bits	18bits	20bits
Sample Rate	200Hz	200Hz	200Hz
Sample Sync	0.05ms	0.2ms	1.0ms
Reference Time	1.0ms	0.5ms	

#### **Potential Improvements**

- Other specifications frequency response, dynamic range, cross-axis sensitivity, sensor layout
- Improved simulations non-uniform stiffness; vary damping ratios, combo flex-shear shapes, non-linear responses
- Other engineering analyses system identification

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# Support provided by NSF CENS and nees@UCLA









#### Future Publications

BSSA: A quantitative basis for strong-motion instrumentation (12/09)

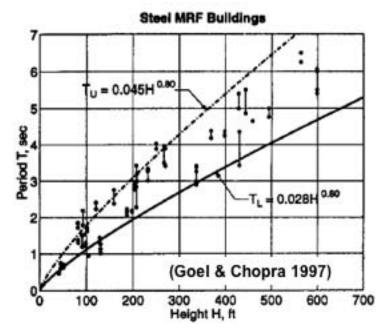
EQS: A quantitative basis for building instrumentation

#### Engineering use of Strong-Motion Response Data

 Traditional – validate modeling assumptions and develop code provisions: fundamental period approximation formulas

Modern – tall building issues, structural health monitoring

(SHM)



# **Tall Building Construction**



- Alternative designs citing Chap 16 of ASCE 7
- NDA of 3D FEM w/ suite of motions & peer review
- Exposed fundamental issues: ground motion selection, modeling guidelines, acceptance criteria
- LA-TBSDC publish document for LA-DBS (2008)
- Since 1965 LA requires accelerographs at base, mid-level, and roof
- UCLA, LA-DBS & CSMIP update requirements
- Deployment approval by peer review panel

Stories	Channels	
10 - 20	15	
20 - 30	21	
30 - 50	24	
> 50	30	

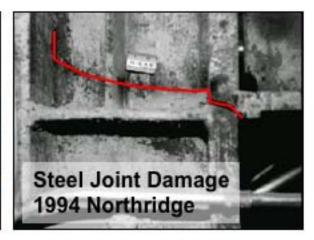
One Rincon Hill - MKA

#### Structural Health Monitoring (SHM)

- Assess health of instrumented structures from measurements
- Detect damage before reaching critical state and allow for rapid post-event assessment
  - Potentially replacing expensive visual inspection which is impractical for wide spread damage in urban areas







# Strong Motion Instrumentation Programs (SMIP)

- CSMIP (CGS), ANSS & NSMP (USGS), K-net/KiK-net (Japan), Taiwan Seismology Center (CWB)
- Provide real-time ShakeMaps and data for engineers and scientists to improve hazard mitigation
- Since early 20<sup>th</sup> century with focus on ground monitoring
- Uniform structural instrumentation specifications are lacking

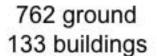




650 ground 170 buildings









92 ground 51 buildings

#### Intensity Measures (IM)

- PGA Peak Ground Acceleration
- PGV Peak Ground Velocity
- PSA Peak Response Spectral Pseudo-Acceleration
- MMI Modified Mercalli Intensity

#### Engineering Demand Parameters (EDP)

- PFA Peak Floor Acceleration
- PID Peak Interstory Drift

#### Advanced Engineering Analyses

- SID System Identification, Model Updating
- SHM Structural Health Monitoring

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